

# Symplectic scheme and the Poynting vector in the reverse time migration

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- To develop a numerical solution for the acoustic wave equation and obtain the wavefield and its time derivative at the same time step.
- The proposed method applications:
  - Vector Poynting computation;
  - Wavefield separation;
  - Boundary condition problem;
  - Common imaging gathers (CIGs);
  - RTM low frequency noise attenuation.

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- In mathematics, a symplectic integrator is a numerical integration scheme for a specific group of differential equations related with classical mechanics and symplectic geometric (Yoshida, 1990).
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The constant density acoustic wave equation

$$\frac{\partial^2 P}{\partial t^2} = c^2 \nabla^2 P, \quad (1)$$

Hamiltonian formulation of the wave equation

$$\begin{aligned} \frac{\partial P}{\partial t} &= Q, \\ \frac{\partial Q}{\partial t} &= c^2 \nabla^2 P. \end{aligned} \quad (2)$$

## Leapfrog (Bonomi et. al, 1998)

$$\begin{aligned}Q^{(n+\frac{1}{3})} &= Q^{(n)} + \frac{1}{6}\Delta tc^2\nabla^2 P^{(n)}, \\P^{(n+\frac{1}{2})} &= P^{(n)} + \frac{1}{2}\Delta tQ^{(n+\frac{1}{3})}, \\Q^{(n+\frac{2}{3})} &= Q^{(n+\frac{1}{3})} + \frac{2}{3}\Delta tc^2\nabla^2 P^{(n+\frac{1}{2})}, \\P^{(n+1)} &= P^{(n+\frac{1}{2})} + \frac{1}{2}\Delta tQ^{(n+\frac{2}{3})}, \\Q^{(n+1)} &= Q^{(n+\frac{2}{3})} + \frac{1}{6}\Delta tc^2\nabla^2 P^{(n+1)}.\end{aligned}\tag{3}$$

## Störmer-Verlet method (Chen, 2009)

$$\begin{aligned}Q^{(n+\frac{1}{2})} &= Q^{(n)} + \frac{1}{2}\Delta t G(P^{(n)}), \\P^{(n+1)} &= P^{(n)} + \Delta t Q^{(n+\frac{1}{2})}, \\Q^{(n+1)} &= Q^{(n+\frac{1}{2})} + \frac{1}{2}\Delta t G(P^{(n+1)}). \end{aligned} \quad (4)$$

where

$$G(P^{(n)}) = -c^2 F^{-1}[k^2 F(P^{(n)})] + 2 \sum_{j=2}^J \frac{(\Delta t)^{2j-2}}{(2j)!} \frac{\partial^{2j} P^{(n)}}{\partial t^{2j}}. \quad (5)$$

Necessary and sufficient condition (Skell et al., 1997).

$$\begin{bmatrix} \frac{\partial P^{(n+1)}}{\partial P^{(n)}} & \frac{\partial P^{(n+1)}}{\partial Q^{(n)}} \\ \frac{\partial Q^{(n+1)}}{\partial P^{(n)}} & \frac{\partial Q^{(n+1)}}{\partial Q^{(n)}} \end{bmatrix}^T [J] \begin{bmatrix} \frac{\partial P^{(n+1)}}{\partial P^{(n)}} & \frac{\partial P^{(n+1)}}{\partial Q^{(n)}} \\ \frac{\partial Q^{(n+1)}}{\partial P^{(n)}} & \frac{\partial Q^{(n+1)}}{\partial Q^{(n)}} \end{bmatrix} = [J]. \quad (6)$$

Symplectic matrix

$$J = \begin{bmatrix} 0 & I \\ -I & 0 \end{bmatrix}. \quad (7)$$

Analytical solution of equation (1) (Pestana and Stoffa, 2010)

$$P(t + \Delta t) + P(t - \Delta t) = 2 \cos(L\Delta t)P(t), \quad (L^2 = -c^2\nabla^2) \quad (8)$$

Using the REM (Kosloff et al., 1989) in (8)

$$P(t - \Delta t) + P(t + \Delta t) = 2 \sum_{k=0}^M C_{2k} J_{2k}(\Delta t R) Q_{2k} \left( \frac{iL}{R} \right) P(t), \quad (9)$$

where

$$R = c_{max} \sqrt{\left( \frac{\pi}{\Delta x} \right)^2 + \left( \frac{\pi}{\Delta y} \right)^2 + \left( \frac{\pi}{\Delta z} \right)^2} \quad (10)$$

The summation can be safely truncated with a  $M > R\Delta t$  (Tal-Ezer, 1987).



## Hamiltonian formulation

$$\frac{\partial P}{\partial t} = Q \quad \text{and} \quad \frac{\partial Q}{\partial t} = H(P). \quad (11)$$

## Störmer-Verlet-REM

$$P^{(n+1)} = P^{(n)} + \Delta t Q^{(n)} + \frac{\Delta t^2}{2} H(P^{(n)}),$$
$$Q^{(n+1)} = Q^{(n)} + \frac{\Delta t}{2} [H(P^{(n)}) + H(P^{(n+1)})]. \quad (12)$$

where:

$$H(P^{(n)}) = \frac{2}{(\Delta t)^2} \left[ \sum_{k=0}^M C_{2k} J_{2k}(\Delta t R) Q_{2k} \left( \frac{iL}{R} \right) - 1 \right] P^{(n)}. \quad (13)$$

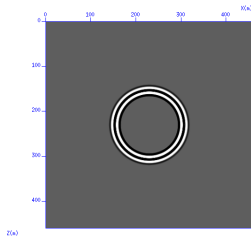
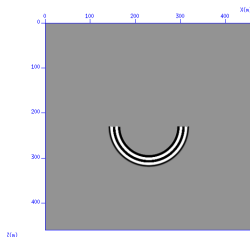
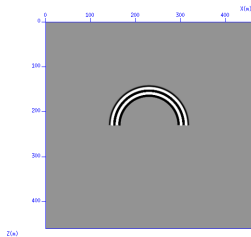
# Poynting vector applications

## Poynting vector

$$\vec{J} = -Q\nabla P \quad (14)$$

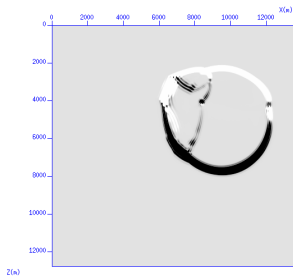
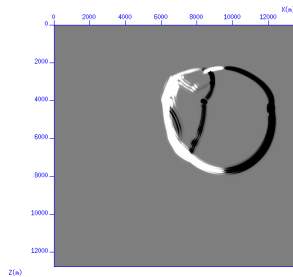
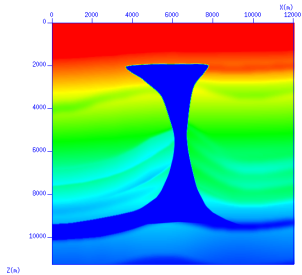
## Wave propagation angle

$$\theta = \arctan\left(\frac{J_z}{J_x}\right) . \quad (15)$$



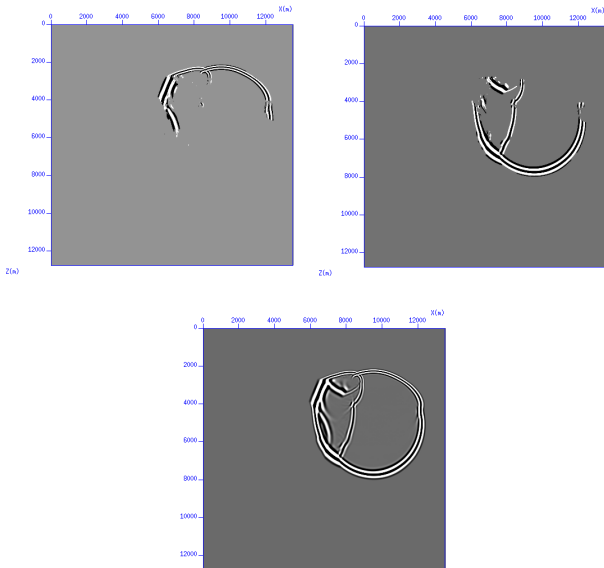
Separated wavefields: Upgoing, downgoing and the original wavefield  
(left to right)

# Poynting vector applications

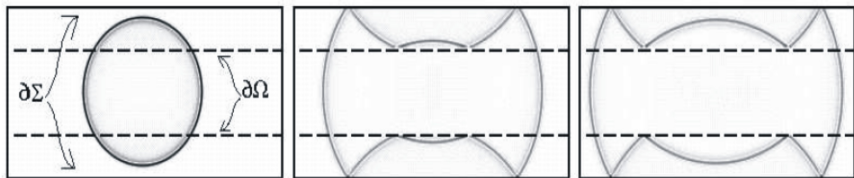


BP Model and snapshot of  $J_x$  (top) and snapshot of  $J_z$  (bottom)

# Poynting vector applications



Separated wavefields: Upgoing and downgoing (top) and the original wavefield (bottom)



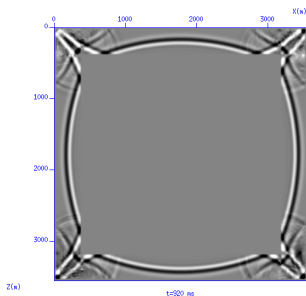
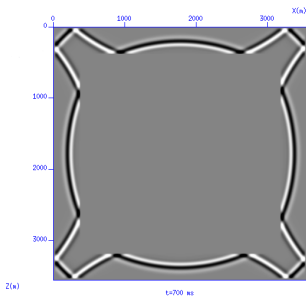
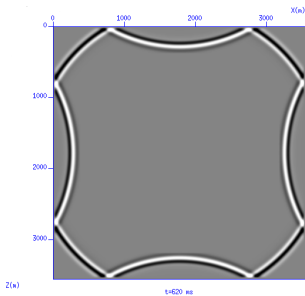
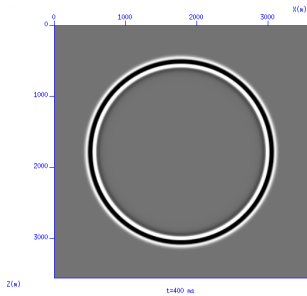
Transparent boundary when the energy leaves  $\partial\Omega$  and reflective boundary when the energy returns to  $\partial\Omega$  (Bonomi e Enrico, 2001).

*Qreverse* (Bonomi e Enrico, 2001)

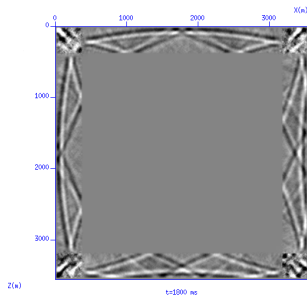
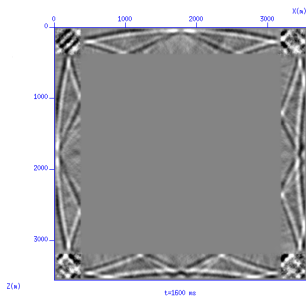
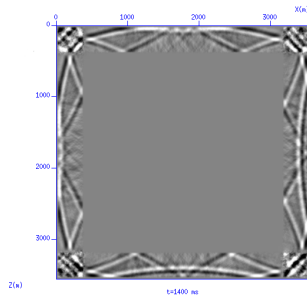
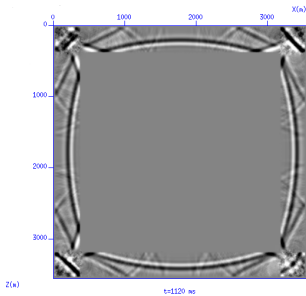
$$\text{For } (x,y,z) \in \partial\Omega \quad \text{where} \quad \vec{j} \cdot \hat{n} < 0 \quad (16)$$

$$\text{Do} \quad Q(x, y, z, t) \leftarrow -Q(x, y, z, t). \quad (17)$$

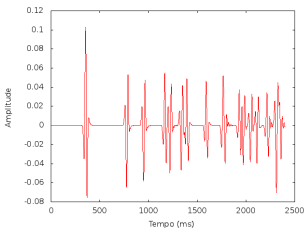
# Qreverse - Snapshots at different instants



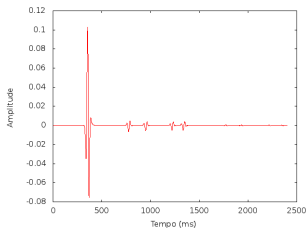
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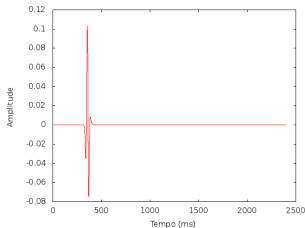
# Qreverse - Trace inside the model



(a)



(b)



(c)

Seismic trace without qreverse (a); with taper (b) and qreverse (c)



- In RTM, the cross-correlation imaging condition, which is given by:

$$I_{cc}(\mathbf{x}) = \int P_F(\mathbf{x}, t) P_B(\mathbf{x}, t) dt \quad (18)$$

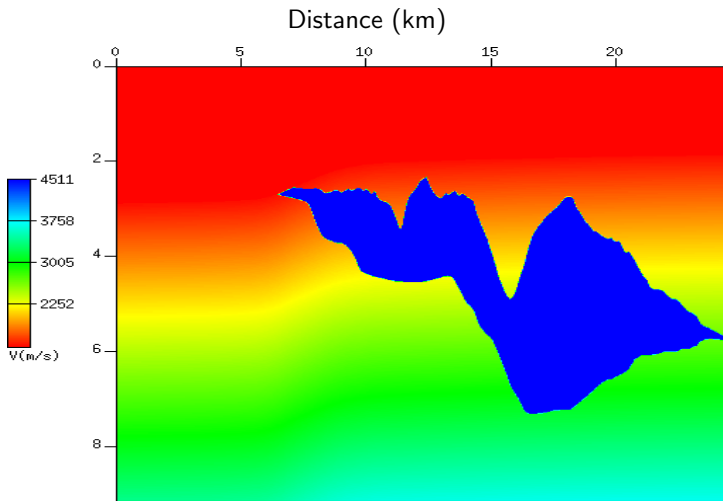
is used in practice and is often preferable due to stability reasons.

- Imaging condition proposed by Bulcão et al. (2007):

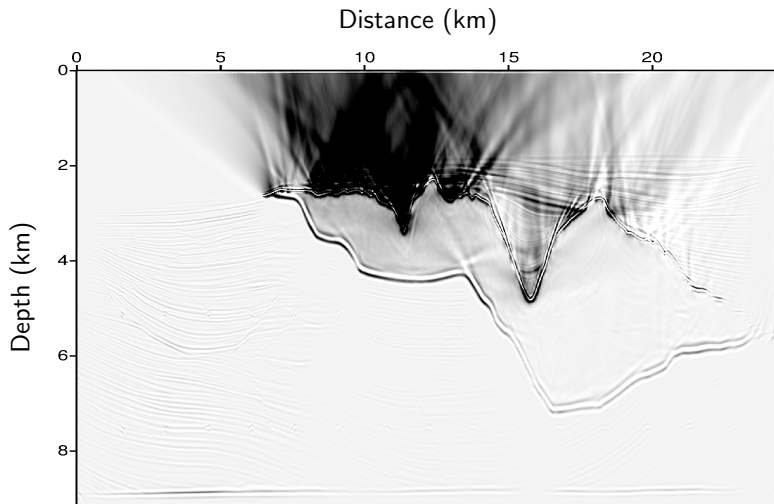
$$I_c(\mathbf{x}) = \sum_{t=0}^{t_f} P_{F_d}(\mathbf{x}, t) P_{B_d}(\mathbf{x}, t) \quad (19)$$

- To avoid the cross-correlation of the downgoing waves with the upgoing waves, which is the cause of the low frequency noise.

# Sigsbee2A velocity model

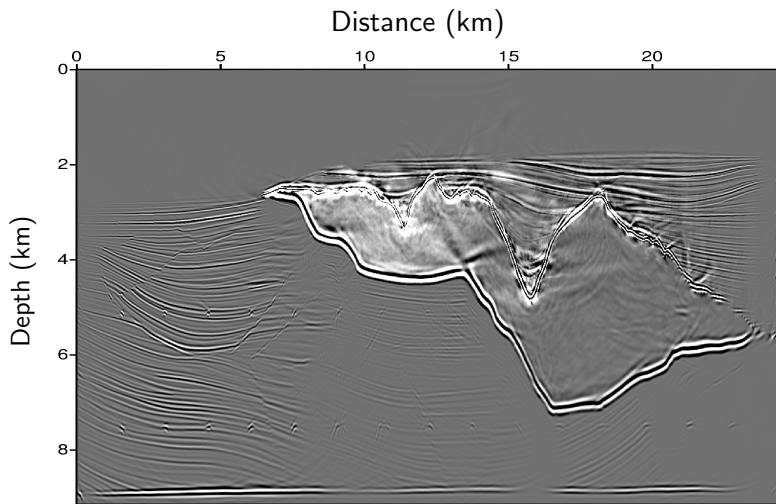


# Pre-stack reverse time migration - SIGSBEE2A model



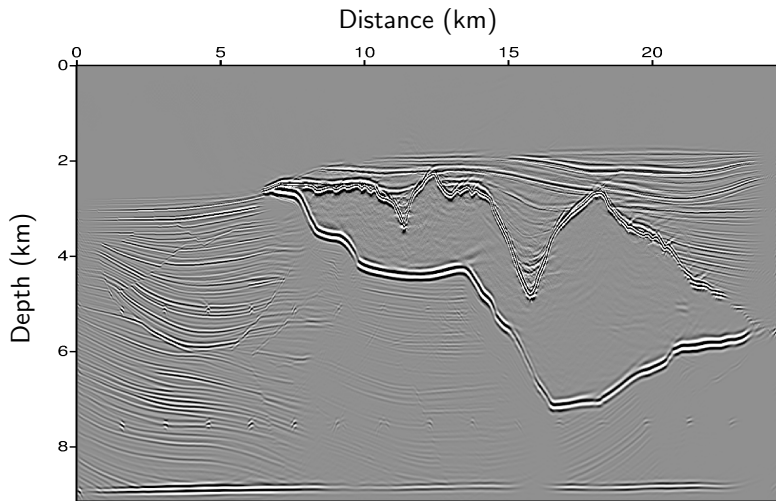
Migration result of the Sigsbee2A dataset - No filtering

# Pre-stack reverse time migration - Sigsbee2A model



Migration result of the Sigsbee2A dataset - Using downgoing source and downgoing receivers parts.

# Pre-stack reverse time migration - Sigsbee2A model



Migration result of the Sigsbee2A dataset - downgoing parts plus high-pass filtering.

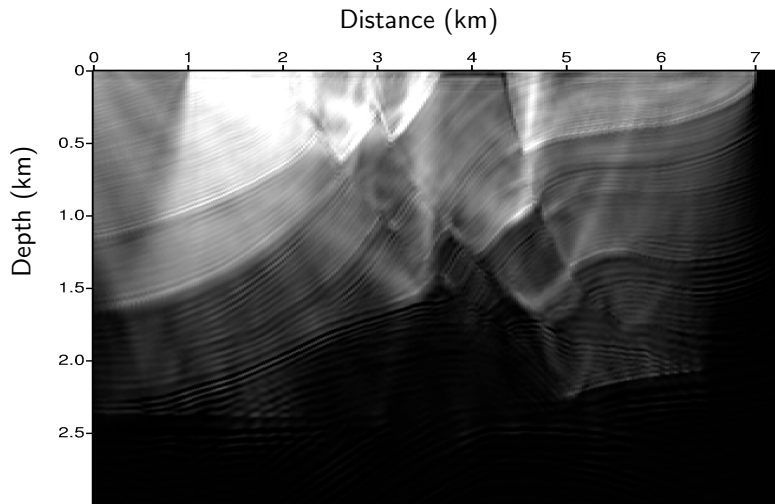
- Cross-correlation imaging condition:

$$I_{cc}(\mathbf{x}) = \int P_F(\mathbf{x}, t) P_B(\mathbf{x}, t) dt$$

- Based on the relationship between inversion and imaging (Luo et al., 2009; Zhou et al., 2009; Whitmore and Crawley, 2012):

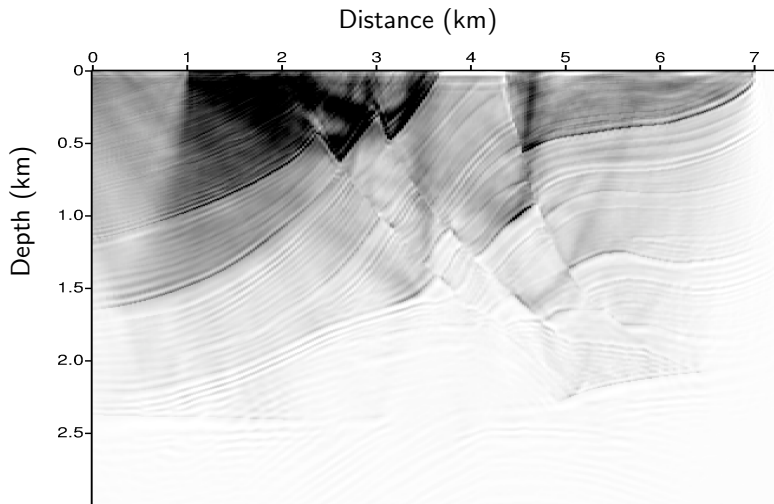
$$\begin{aligned} I_{ii}(\mathbf{x}) &= \frac{1}{v^2(\mathbf{x})} \int \frac{\partial}{\partial t} P_F(\mathbf{x}, t) \frac{\partial}{\partial t} P_B(\mathbf{x}, t) dt \\ &+ \int \nabla P_F(\mathbf{x}, t) \cdot \nabla P_B(\mathbf{x}, t) dt \end{aligned} \quad (20)$$

# Pre-stack RTM result - Marmousi model



Gradient image condition.

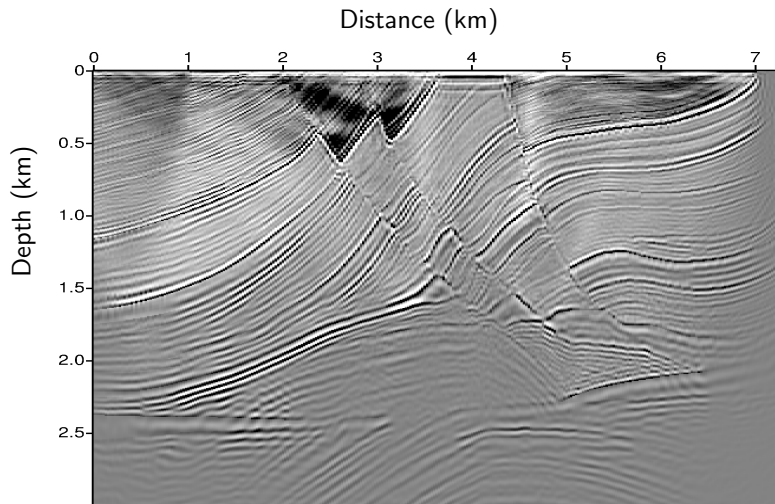
# Pre-stack RTM result - Marmousi model



Time derivative image condition.



# Pre-stack RTM result - Marmousi model



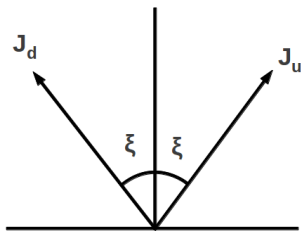
Inverse scattering image condition

# Reflection angle & Common imaging gathers (CIGs)

Reflection angle:

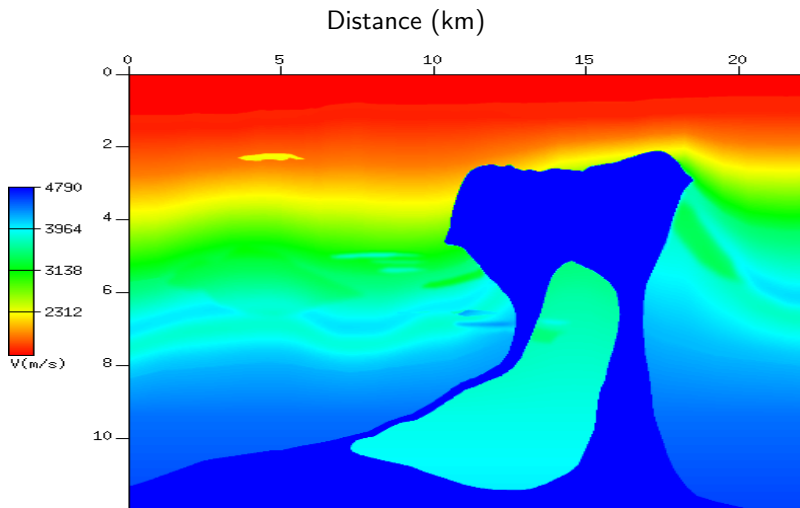
$$\cos(\psi) = \frac{\vec{J}_d \cdot \vec{J}_u}{|\vec{J}_d| |\vec{J}_u|} . \quad (21)$$

$$\psi = 2\xi \quad (\xi\text{- reflection angle}) . \quad (22)$$

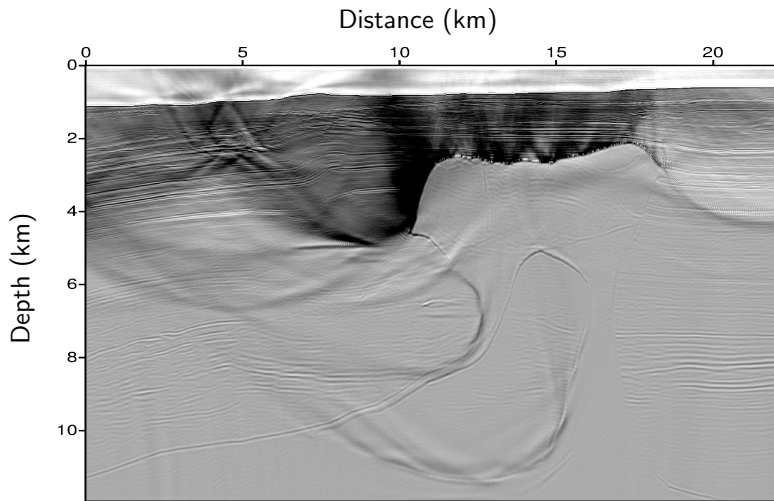


Source Poynting vector ( $\vec{J}_d$ ) and receiver Poynting vector ( $\vec{J}_u$ ).

# 2004 BP velocity model

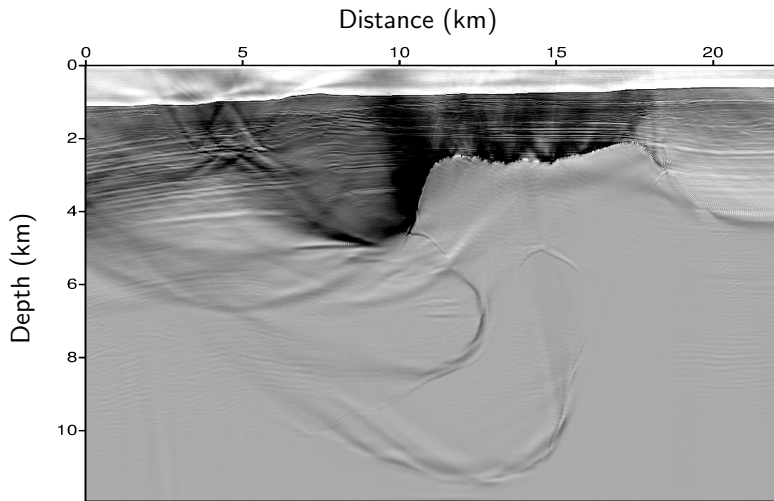


# Pres-stack RTM using CIGs

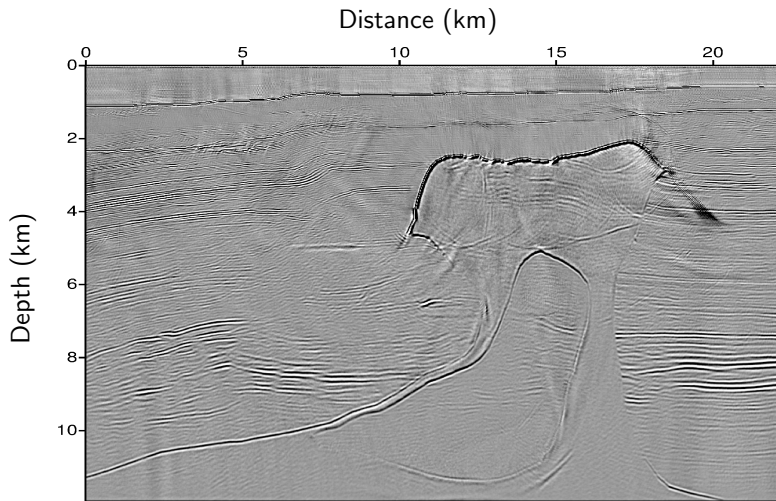


Migration result of the 2004 BP 2D dataset using the CIGs reflection angles from  $0^\circ$  to  $90^\circ$ .

# Pre-stack RTM using CIGs



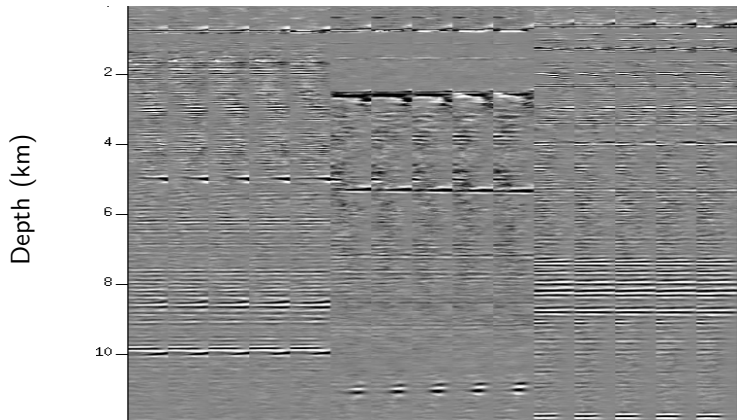
Migration result of the 2004 BP 2D dataset using the CIGs reflection angles from  $61^\circ$  to  $90^\circ$ .



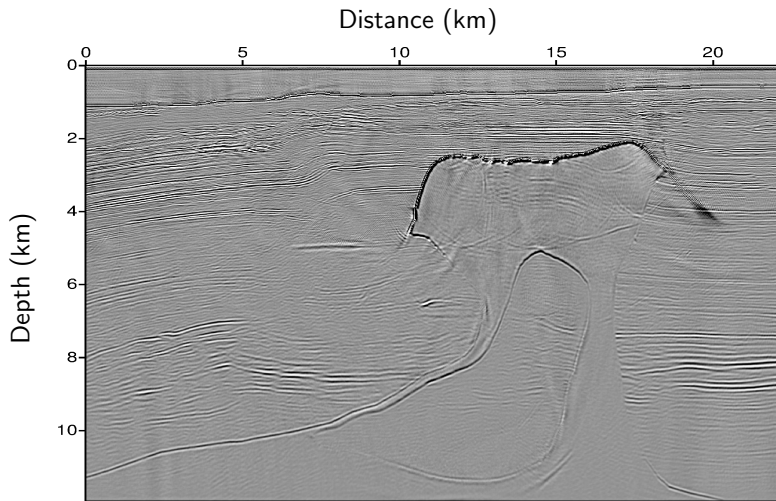
Migration result of the 2004 BP 2D dataset using the CIGs reflection angles from  $0^\circ$  to  $60^\circ$ .

# CIGs in the reflection angle domain from the 2004 BP dataset

Reflection angles from  $0^\circ$  to  $60^\circ$



Some common image gathers from the 2004 BP dataset in the reflection angle domain.



Final migration result obtained by summing the CIGs reflection angles from  $0^\circ$  to  $60^\circ$  and the CIGs reflection angles from  $61^\circ$  to  $90^\circ$  after high-pass filtering.



The new symplectic numerical scheme combined with REM proved to be a good alternative to the following applications:

- Reverse time migration
- Vector Poynting computation;
- Wavefield separation;
- Boundary condition problem;
- Common imaging gathers (CIGs);
- RTM low frequency noise attenuation.

This research was supported by CNPq and INCT-GP/CNPq. The facility support from CPGG/UFBA is also acknowledged.

